

RESPONSE DUE TO HEAVY AIRCRAFT TAKEOFF: ADVANCED MODELING COMPARING SINGLE-TIRE AND DUAL-TANDEM GEAR

Jaime A. Hernandez,
PhD Candidate

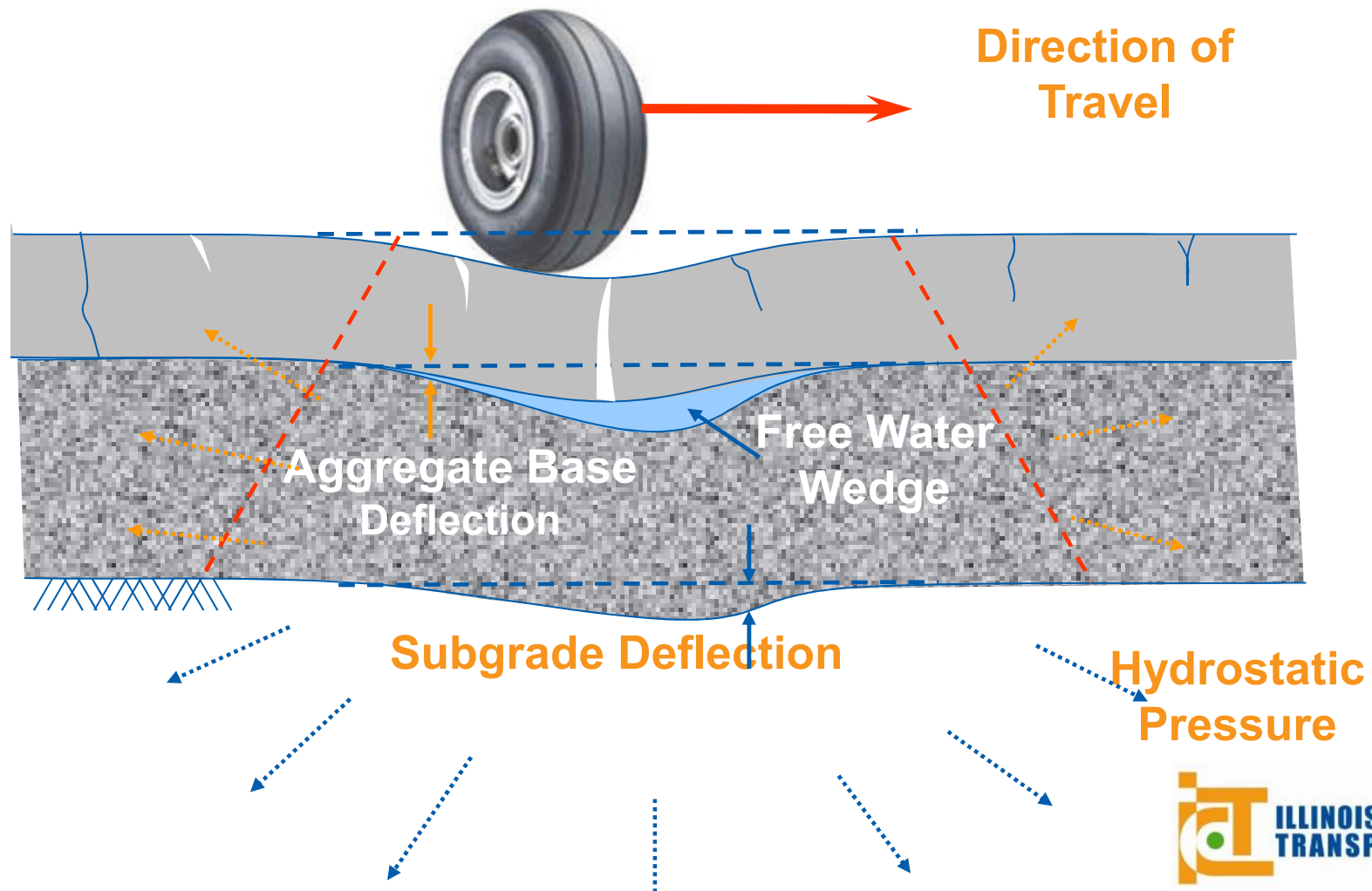
Imad L. Al-Qadi, Phd, PE, Dist.M.ASCE
Founder Professor of Engineering and ICT Director

University of Illinois at Urbana-Champaign

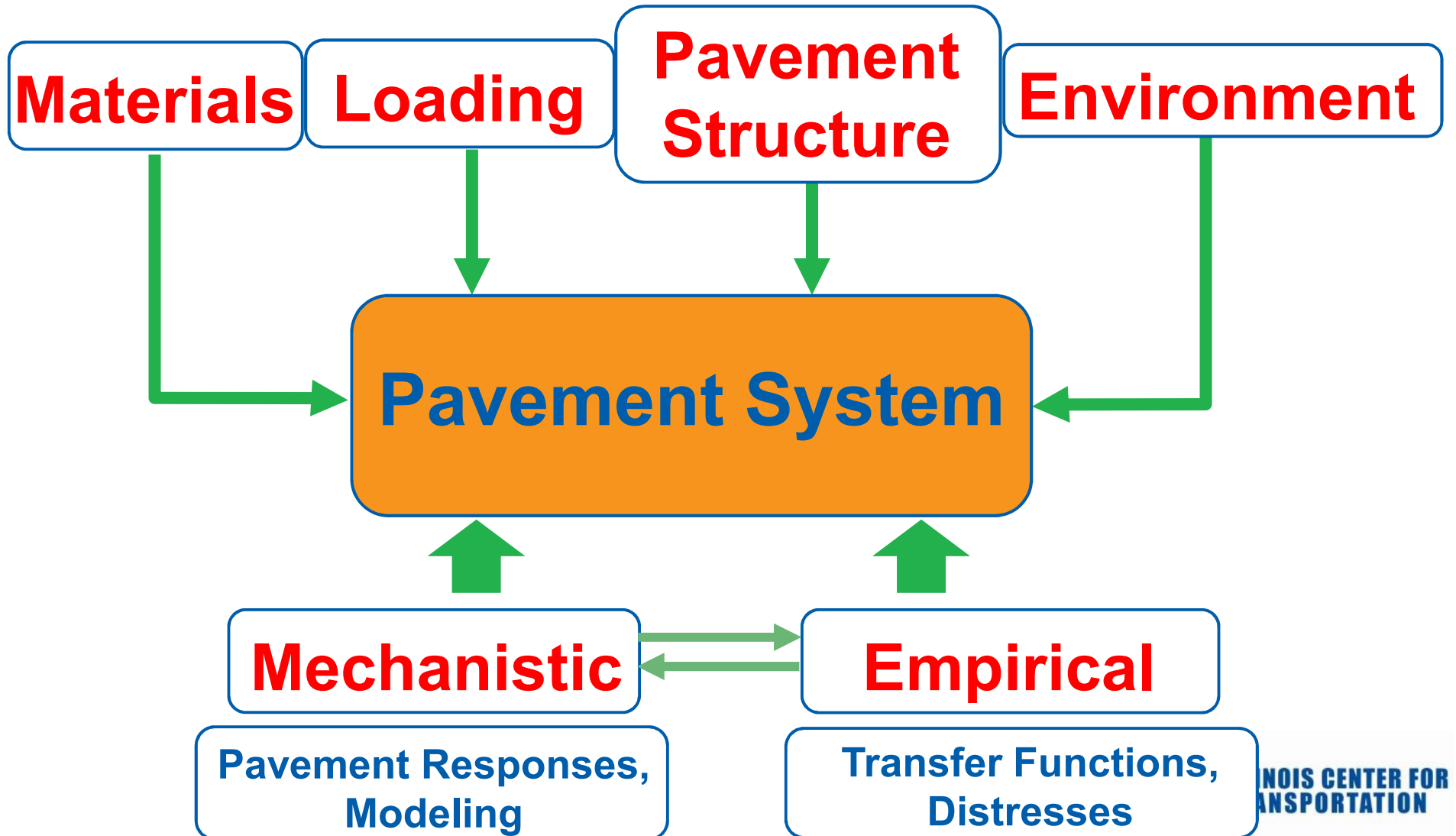
August 5th, 2014



Loaded Flexible Pavement

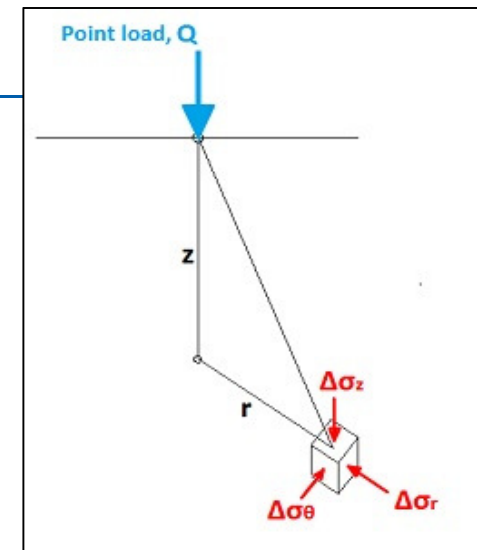


Pavement Design

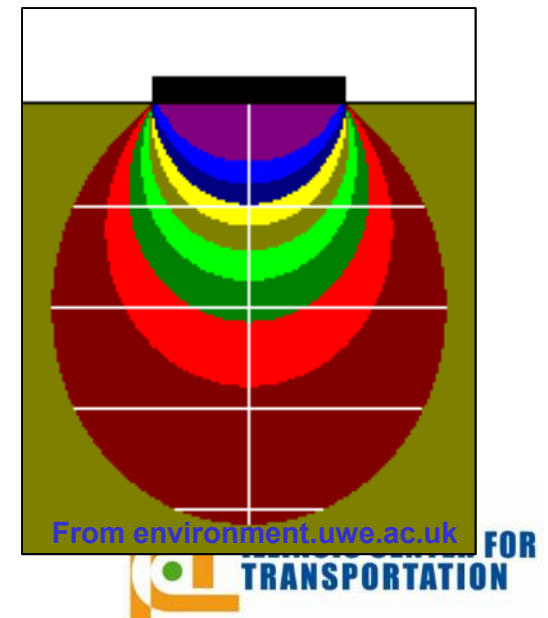


ACN-PCN

- Based on Boussinesq solution
 - Material assumed as elastic homogeneous
 - Solution for half space subjected to a point load
 - By integration another loading cases can be obtained
 - Applicable to multiple layers if modulus ratio is close to 1 or need to be adjusted



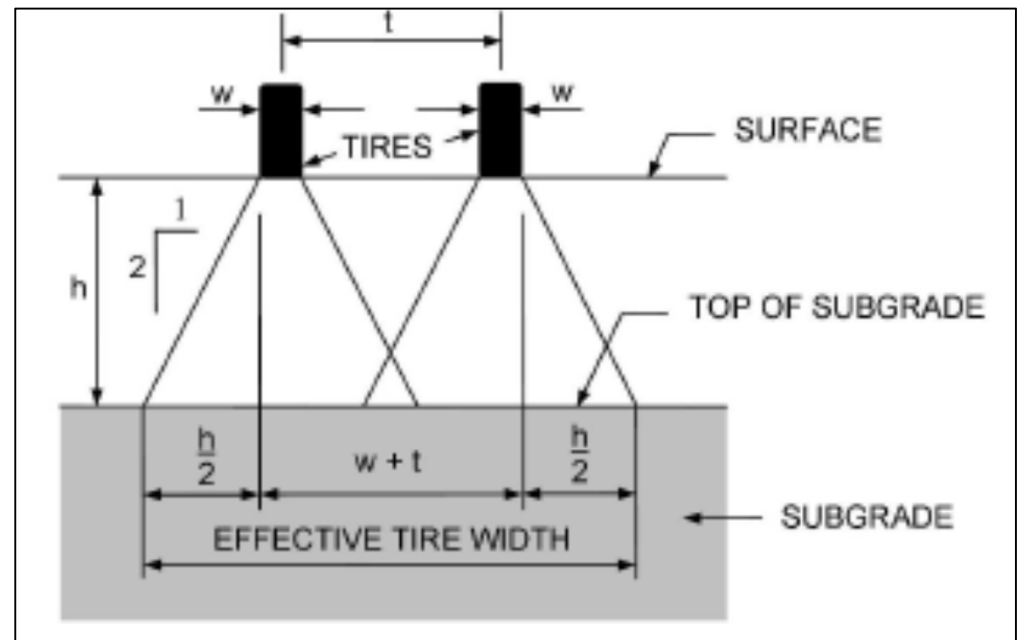
From casio-fx.com



From environment.uwe.ac.uk

Gear Interaction

- Gear interaction effect is based on **effective tire width**
- Effect of **full gear** on responses not considered directly (e.g. 3 duals in tandem)



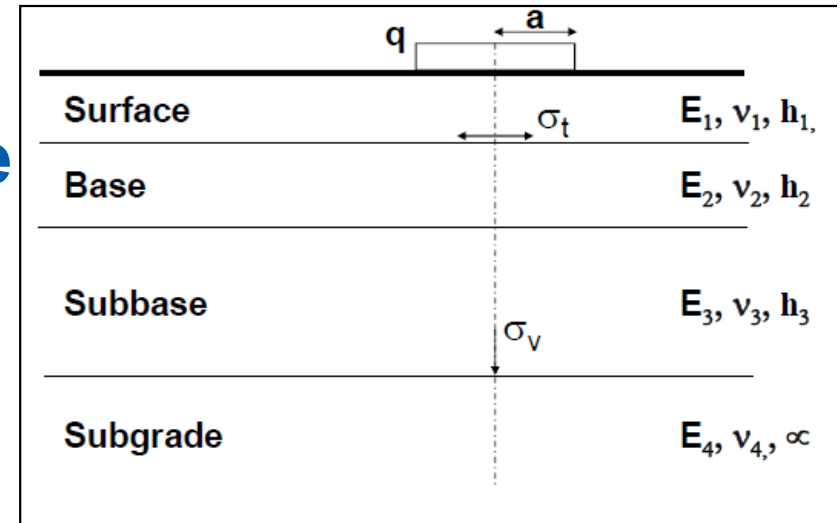
FAA Advisory Circular 150/5320-6E

FAA Design Assumptions

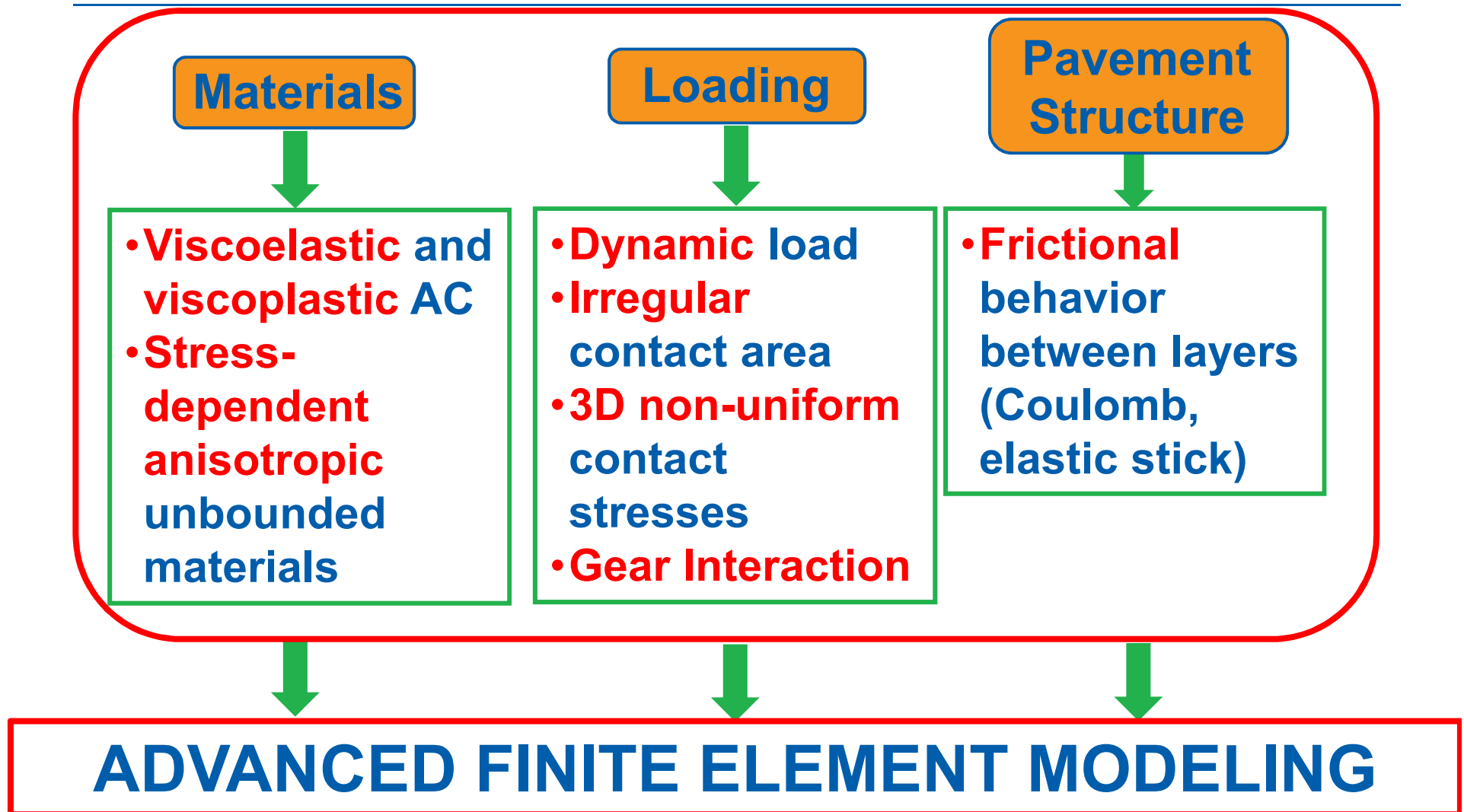
- Design for **20 years** with no maintenances
- **Mixed aircraft traffic**
- **Cumulative damage factor:** based on tensile strain at bottom of AC and vertical strain on subgrade **only**
- Pavement responses: **layered elastic theory**

Layer Elastic Theory (FAARFIELD)

- **Linear elastic** materials
- **Full continuity** at interface
- **Pavement layer: weightless and infinite** in horizontal direction
- **Subgrade: infinite** in both directions
- **Circular** contact area with **uniform vertical** contact stresses

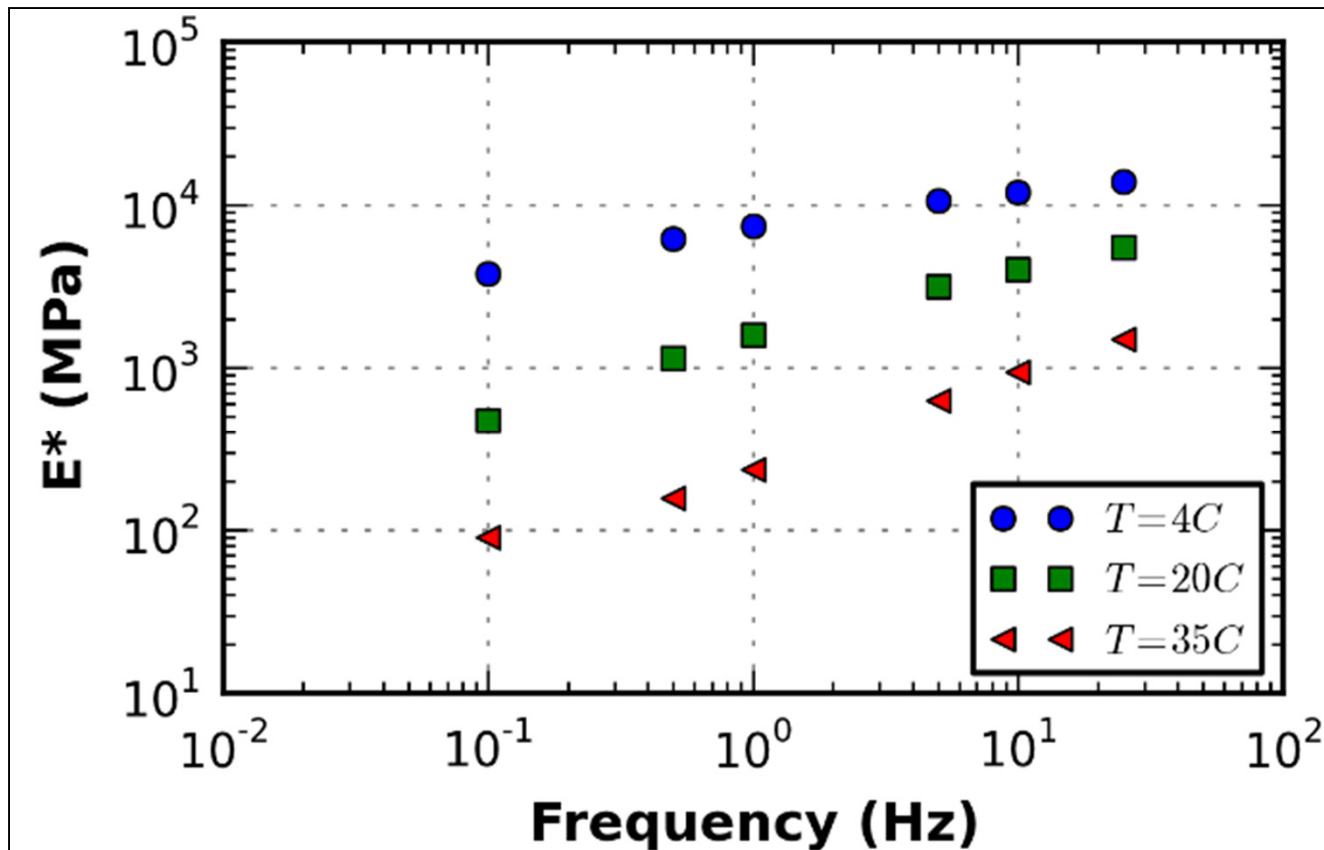


Actual Behavior



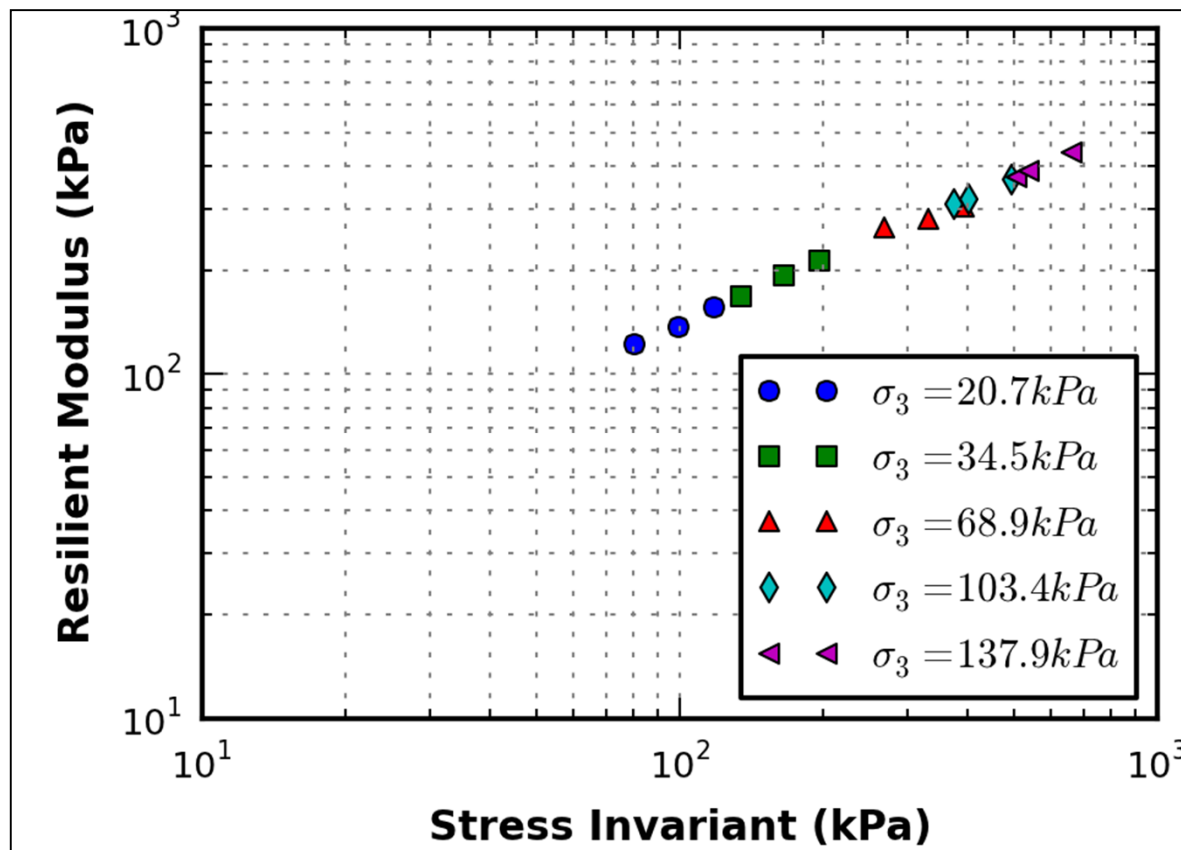
Viscoelastic AC

- Modulus of AC depends on **loading time** and **temperature** (*it is not linear elastic*)



Unbound Material

- Resilient modulus depends on **stress level** and **direction** (*it is not linear elastic*)



Aircraft Loading

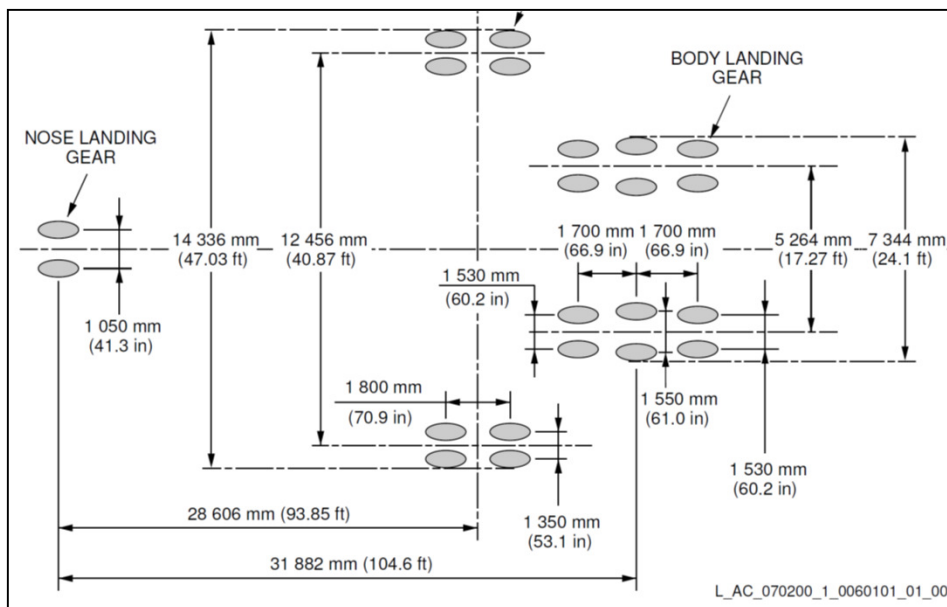
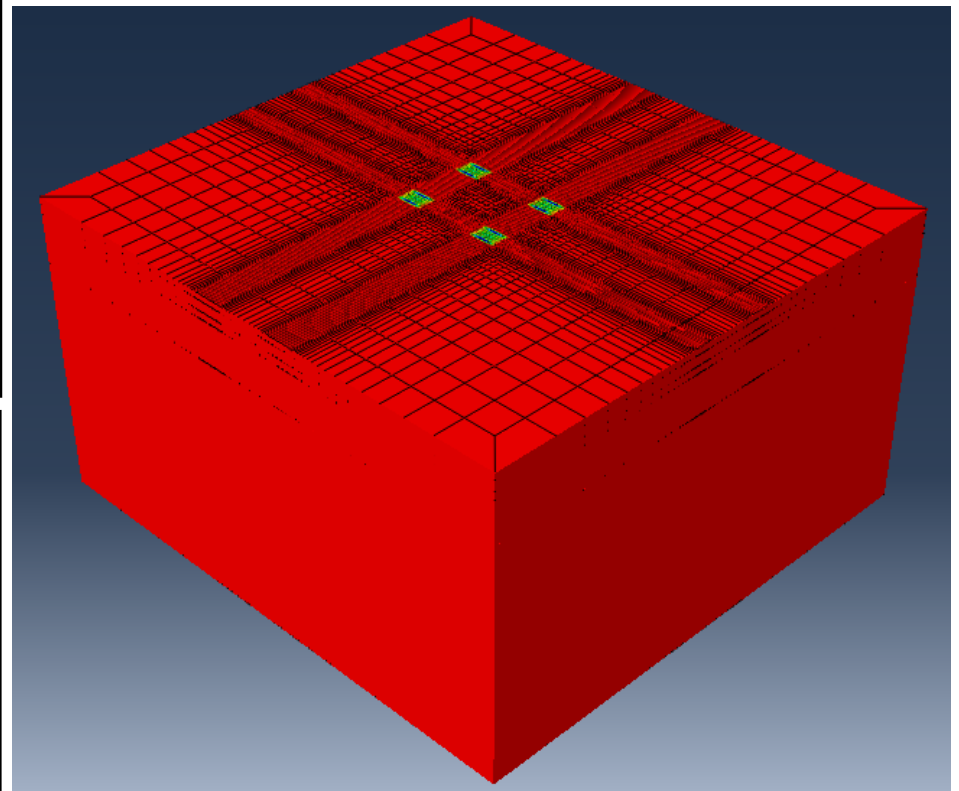
- ❑ **Moving** load (*it is not stationary*)
- ❑ Loading **amplitude** continuously changes
- ❑ **Dynamic tire force** is excited by pavement irregularities (*it is not static*)
- ❑ High tire inflation pressure and load
- ❑ Gear interaction

Heavy Load Modeling: Airbus A-380

http://www.airliners.net/aviation-forums/tech_ops/read.main/253220/1/



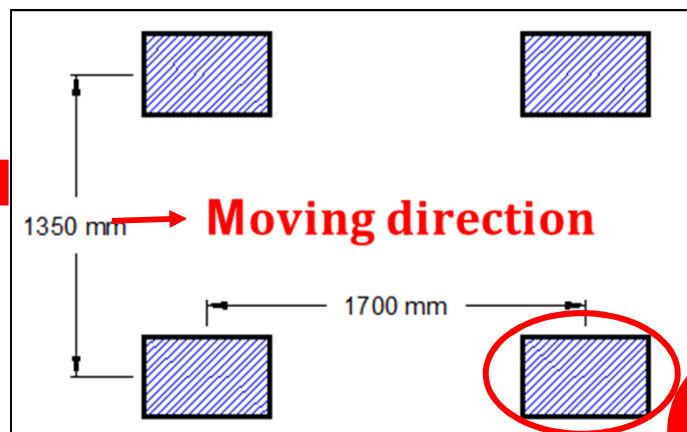
Landing Gear



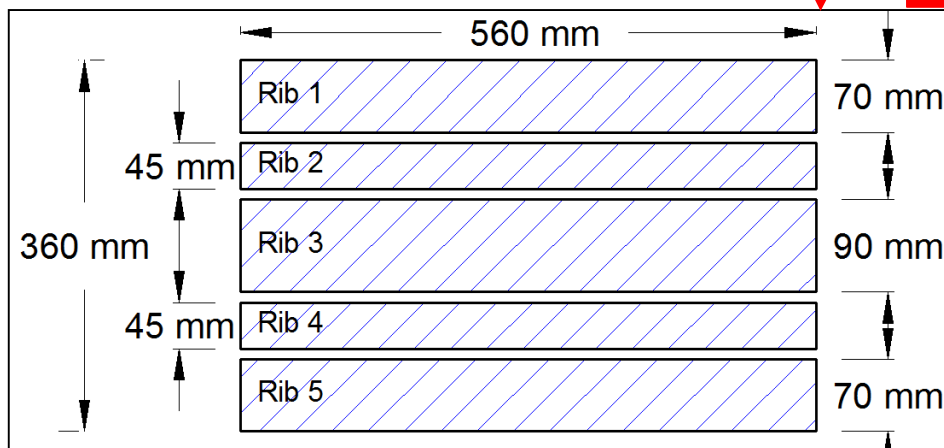
Loading – Stress Distribution

□ Gear configurations

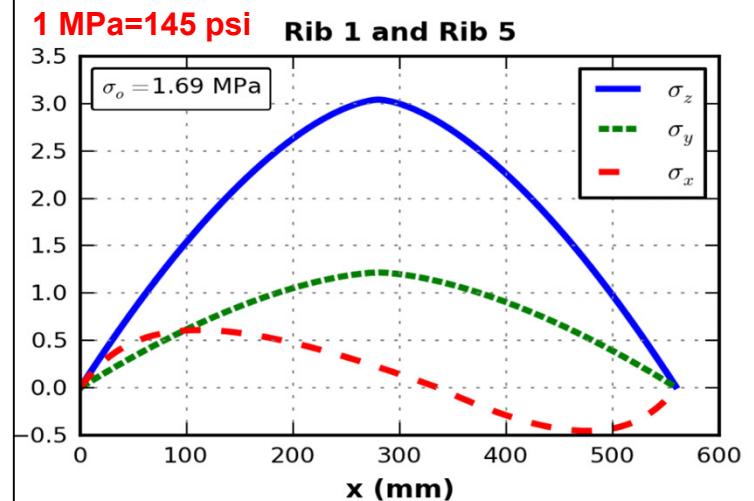
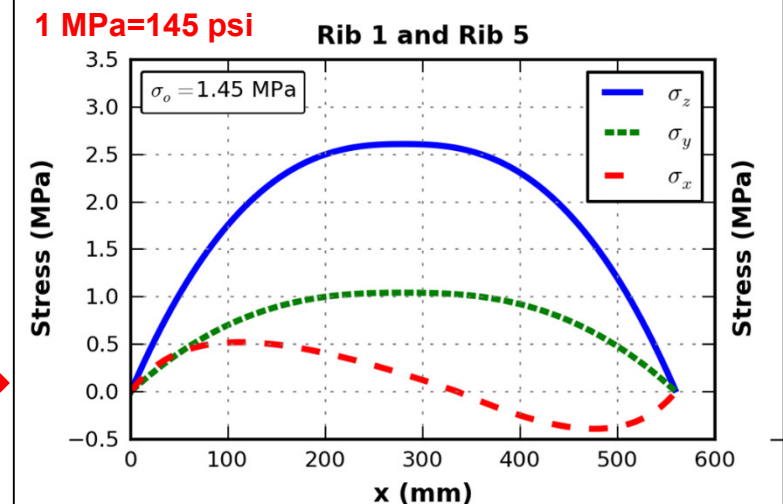
Load
262.1 kN



□ Tire footprint

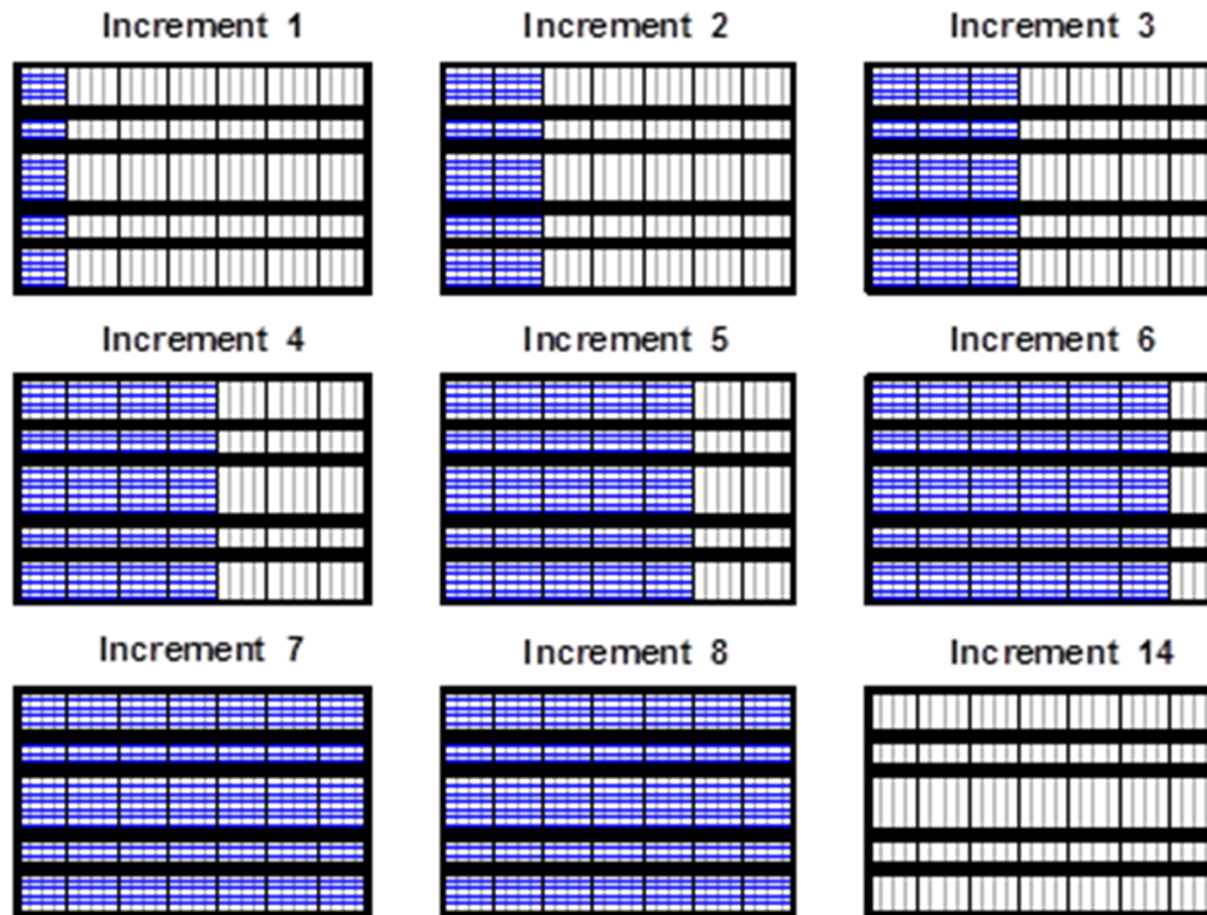


□ 3D contact stresses

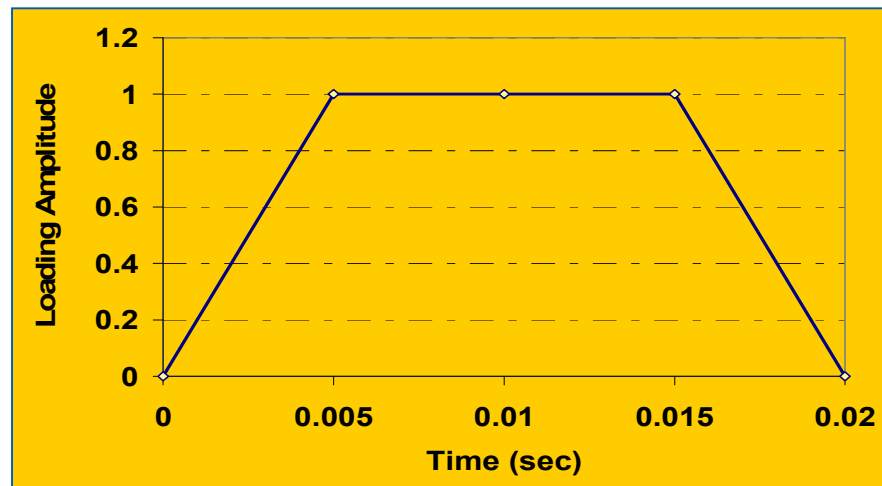


Takeoff

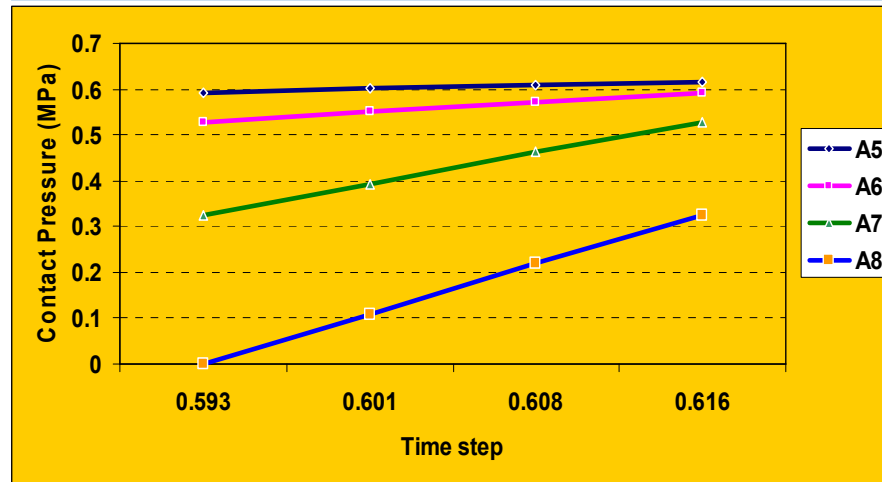
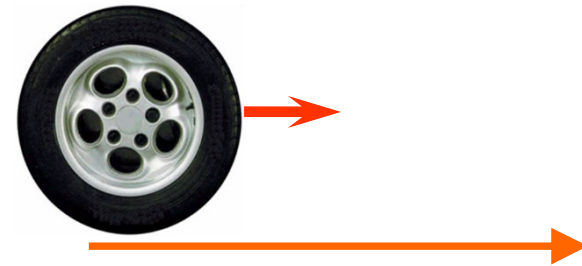
- Contact patch **gradually loaded**



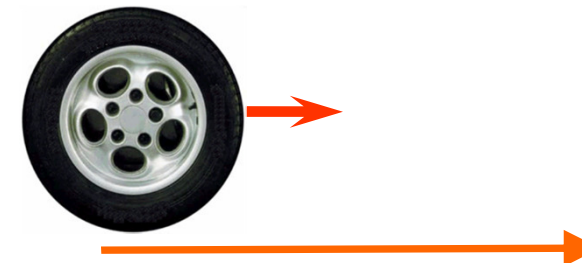
Continuous Moving Loading



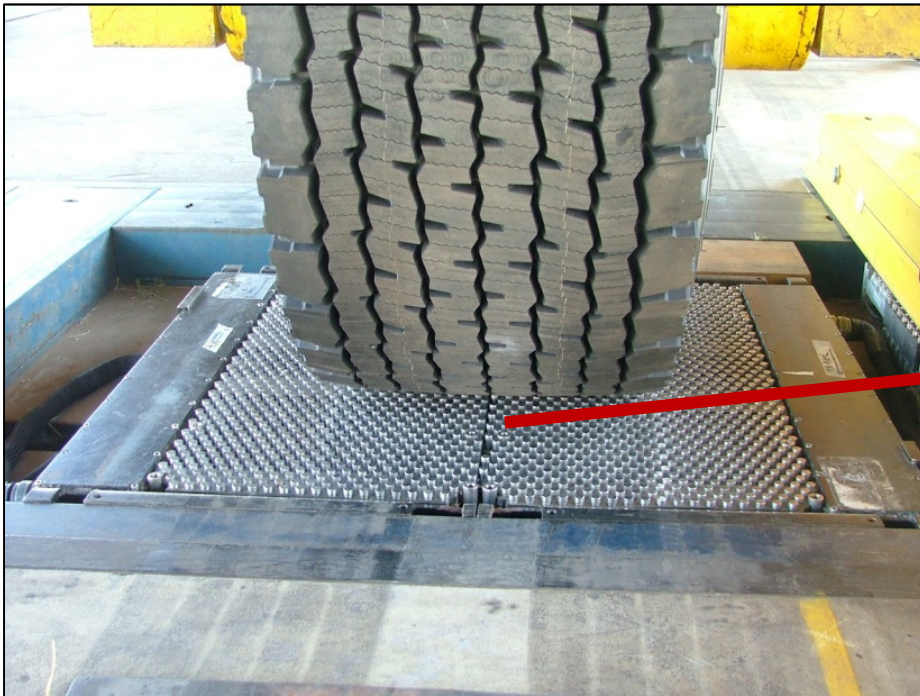
Trapezoidal



Continuous

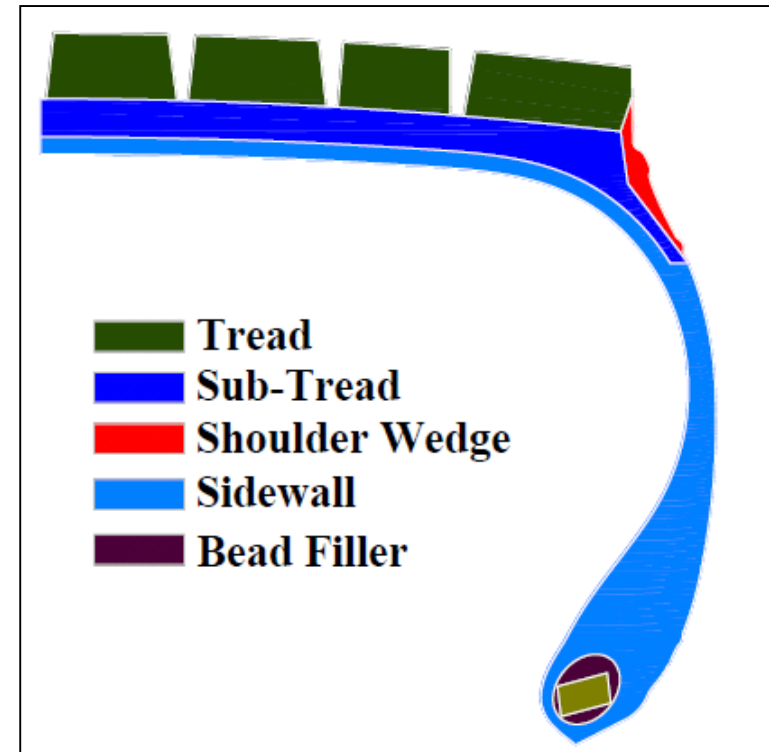


Measurement Contact Stresses



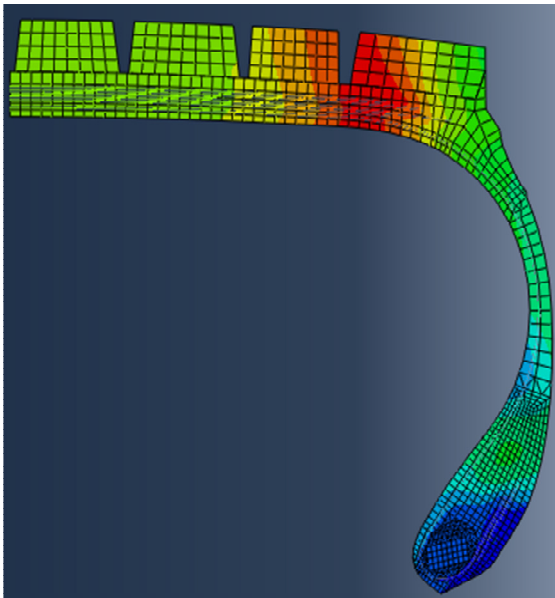
Tire Modeling

- ❑ Measuring contact stresses is cumbersome and expensive
- ❑ Simplified methods needed: **modeling** and **analytical expressions**
- ❑ Tire components: Rubber and Reinforcement

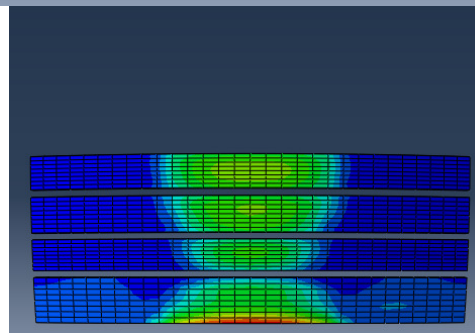
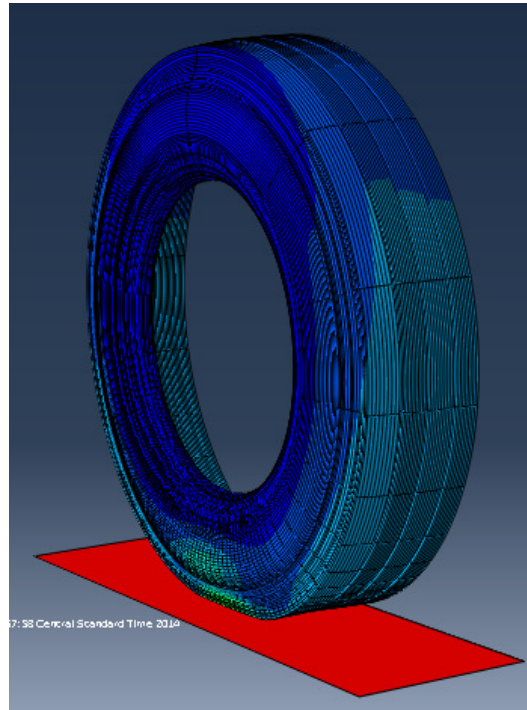


Tire Modeling

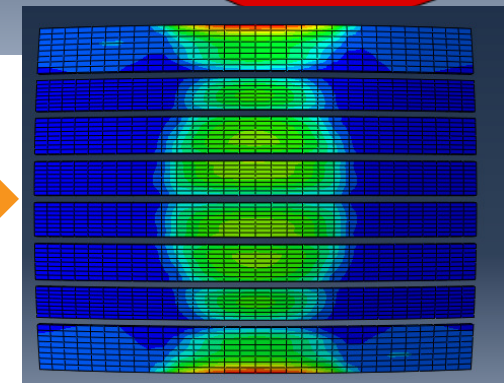
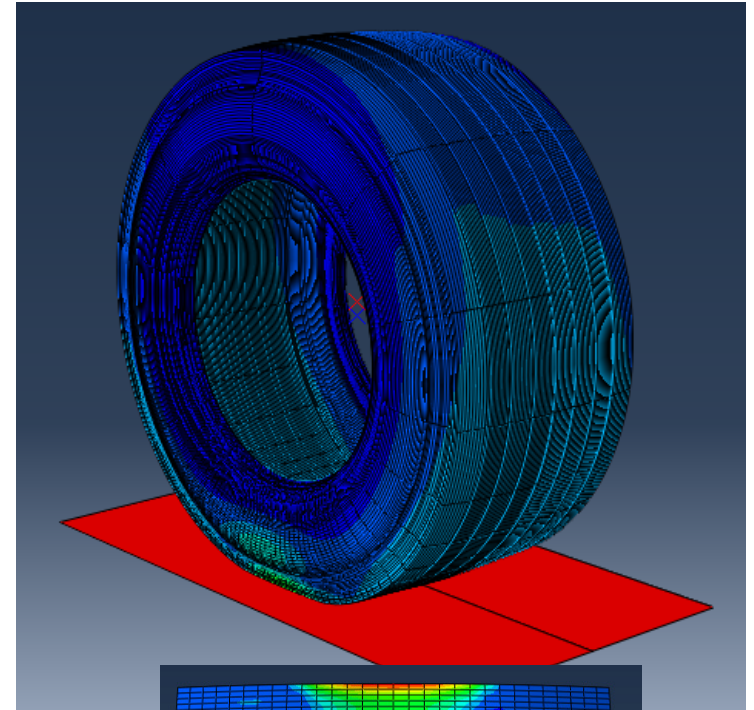
Axisymmetric



Half Tire

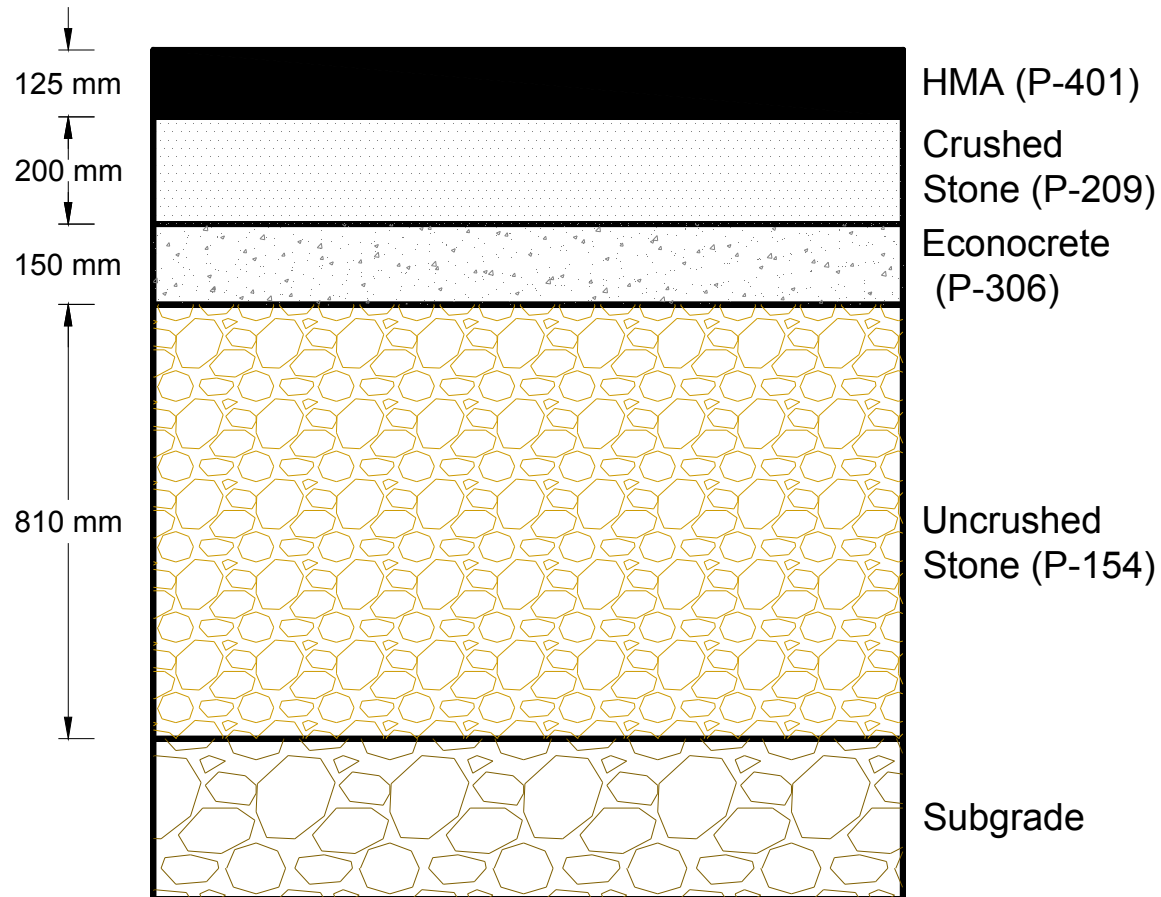


Full Tire



ER FOR
TION

Numerical Modeling NAPTF Section

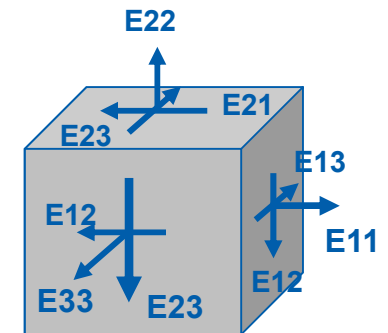


Elastic Modulus for linear elastic analysis

Layer	E (MPa)
AC (P-401)	3151.0
Base (P-209)	518.0
Econocrete (P-306)	4830.0
Uncrushed Stone (P-154)	276.0
Subgrade	36.0

Responses Considered

$\epsilon_{11,ac}$	Longitudinal tensile strain bottom of AC
$\epsilon_{33,ac}$	Transverse tensile strain bottom of AC
$\epsilon_{22,bs}$	Vertical strain base
$\epsilon_{22,sg}$	Vertical strain subgrade
$\epsilon_{23,ac}$	Vertical shear AC
$\epsilon_{23,bs}$	Vertical shear base
$\epsilon_{23,sg}$	Vertical shear subgrade



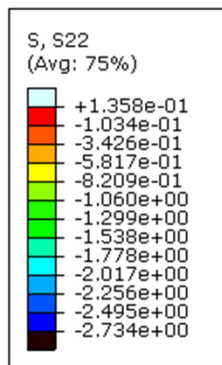
Traffic
Direction



Conventional vs FEM

	WinJULEA	3D FEM	Diff. (%)
$\epsilon_{11,ac}$	377.8	480.2	27.1
$\epsilon_{33,ac}$	377.8	495.3	31.1
$\epsilon_{22,bs}$	1893.7	3052.8	61.2
$\epsilon_{22,sg}$	547.9	557.0	1.7
$\epsilon_{23,ac}$	196.5	200.1	1.8
$\epsilon_{23,bs}$	734.4	350.3	-52.3
$\epsilon_{23,sg}$	189.6	108.5	-42.8

Modeling Results



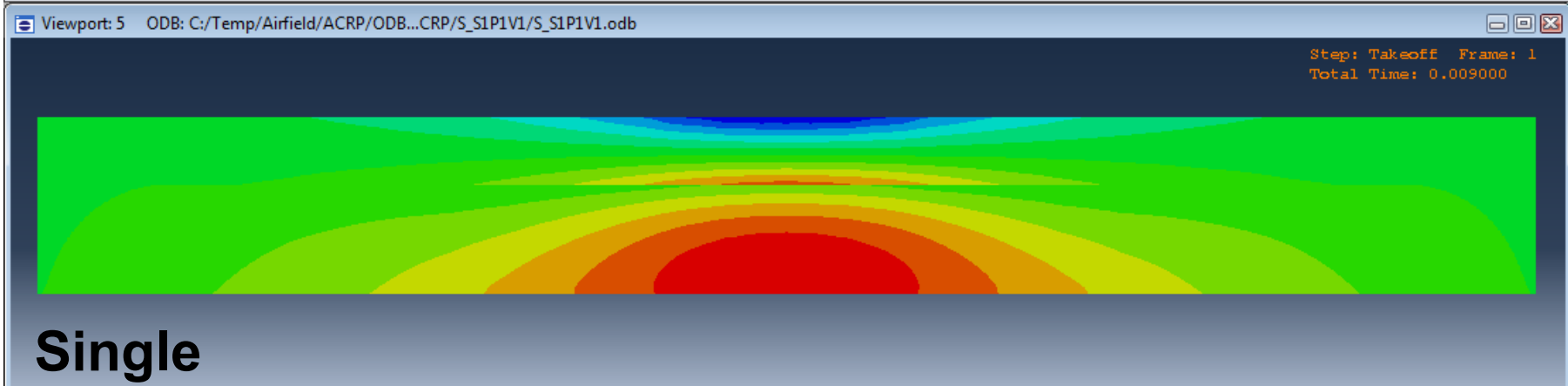
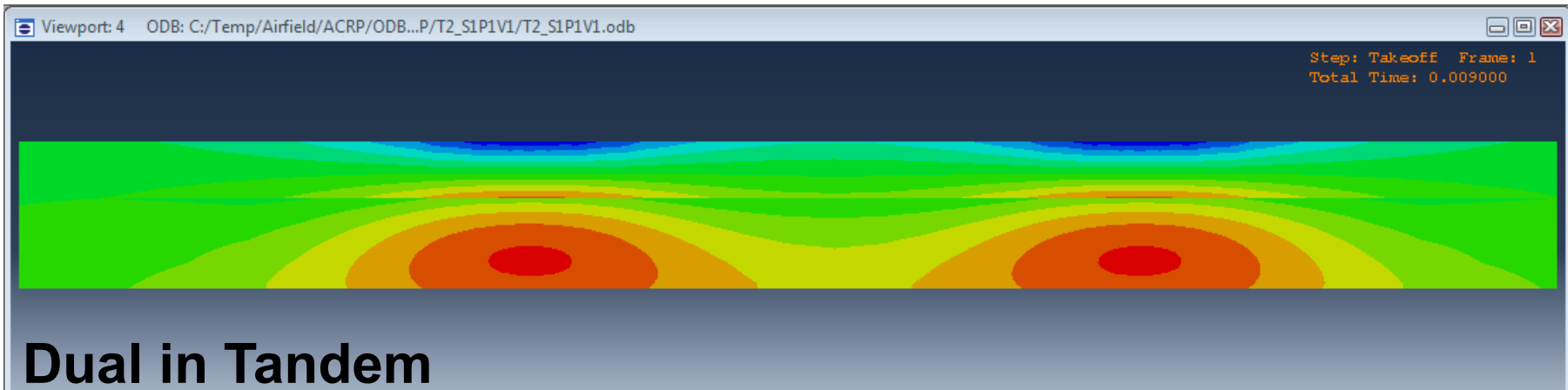
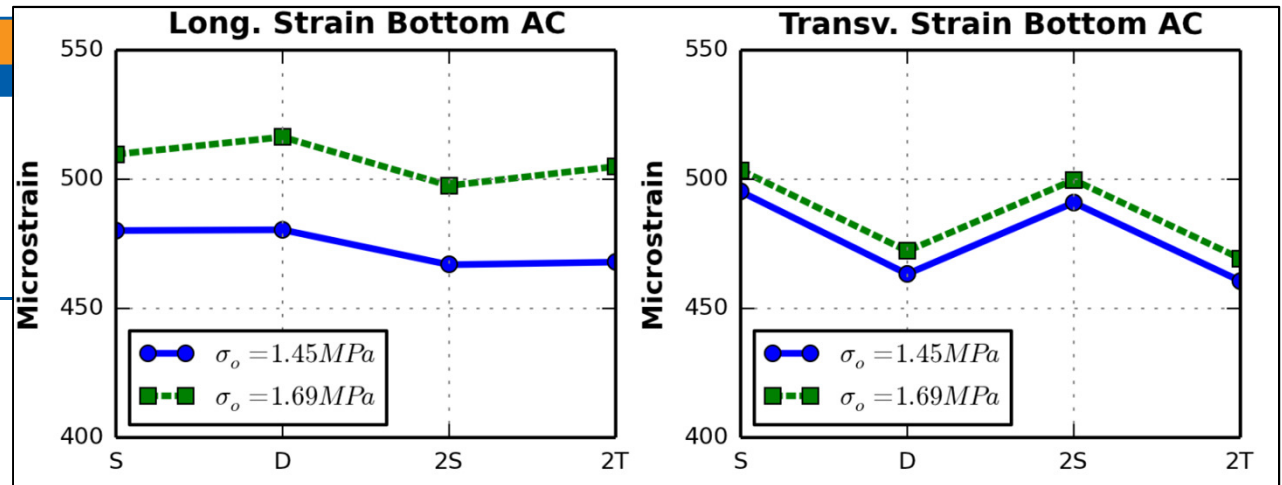
Step: Approach Frame: 0
Total Time: 0.000000



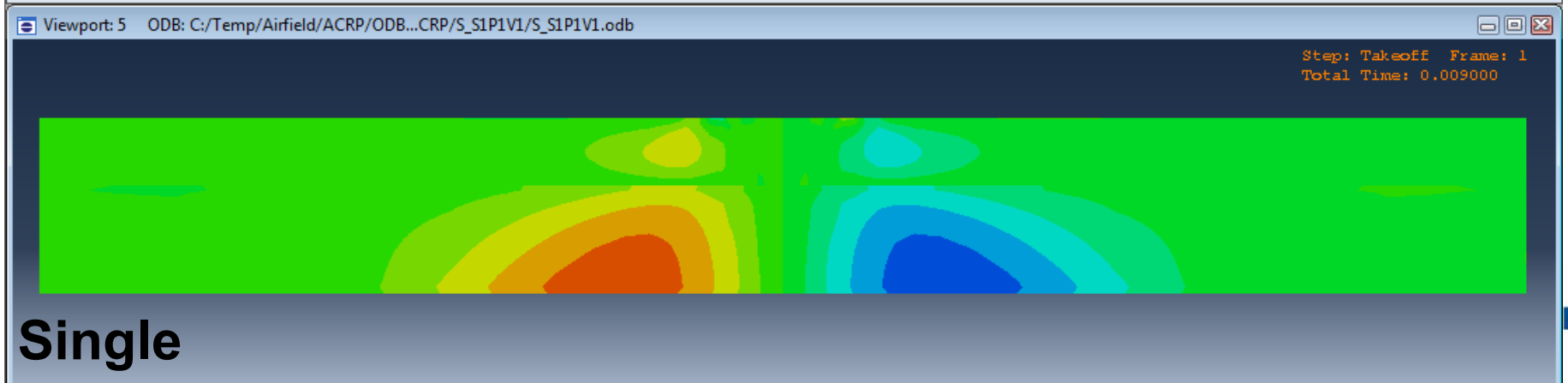
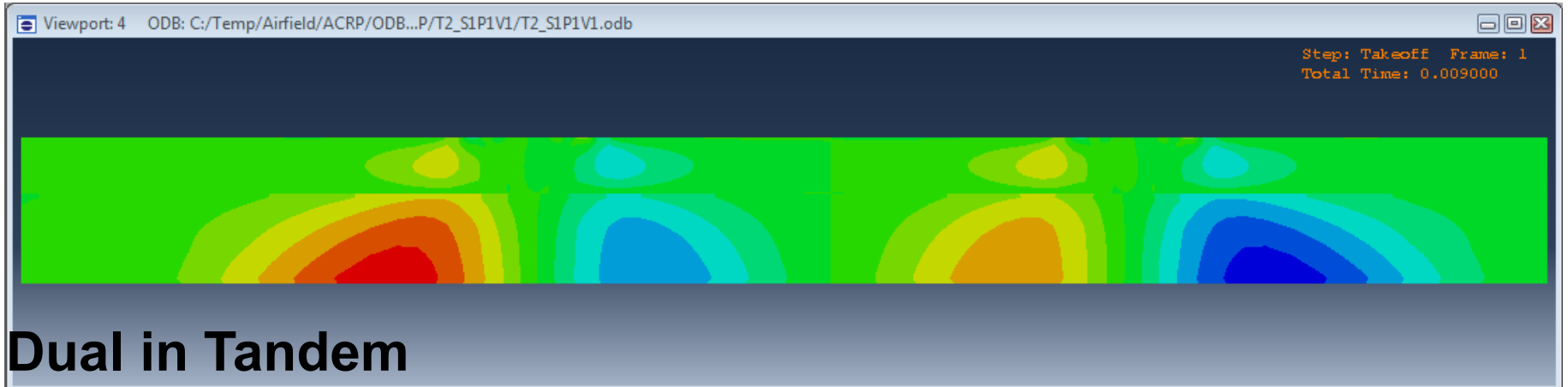
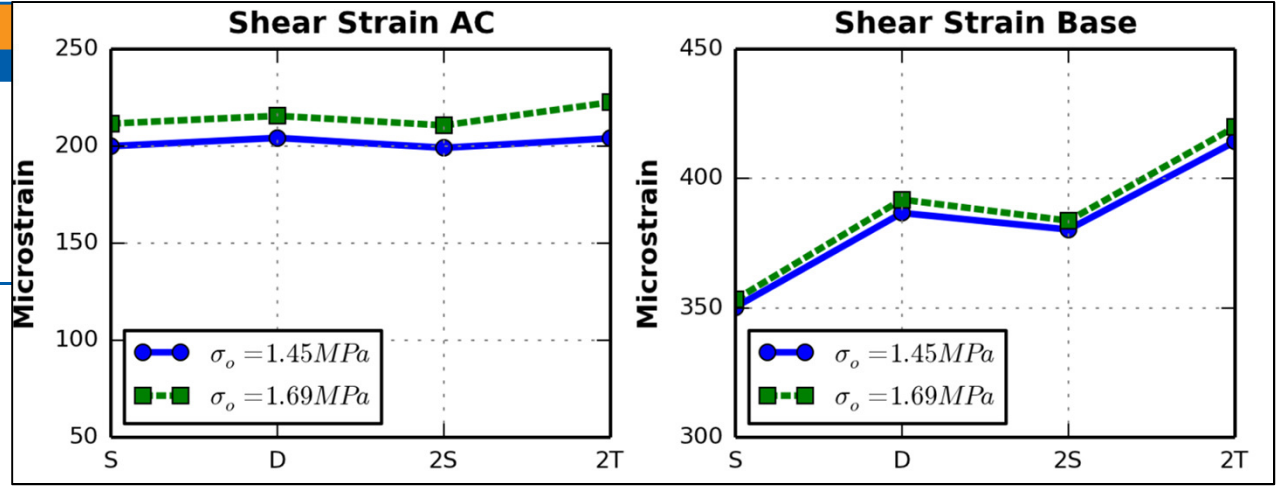
ODB: T2_S1P1V1.odb Abaqus/Standard 6.11-2 Fri Dec 27 17:01:13 Central Standard Time 2013

Step: Approach
Increment: 0: Step Time = 0.000
Primary Var: S, S22

Strain at Bottom of AC

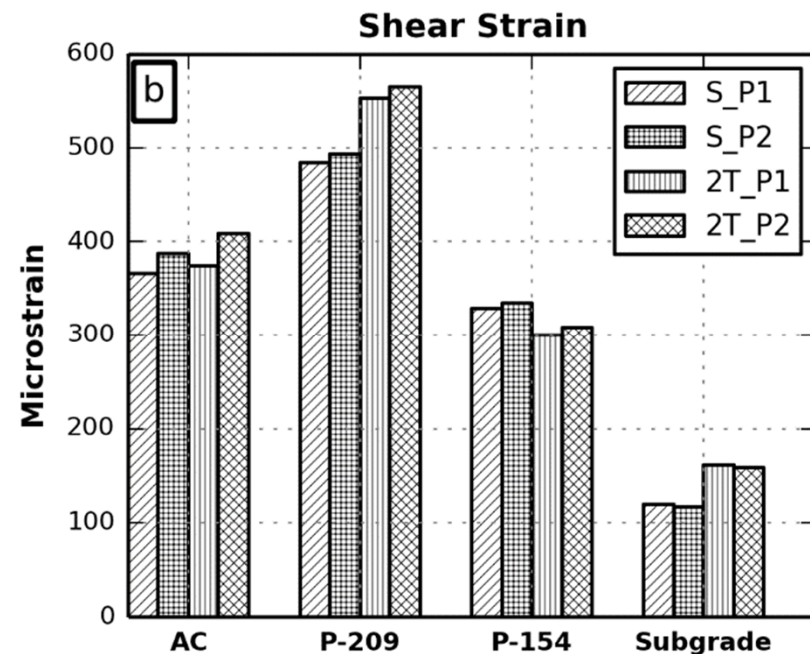
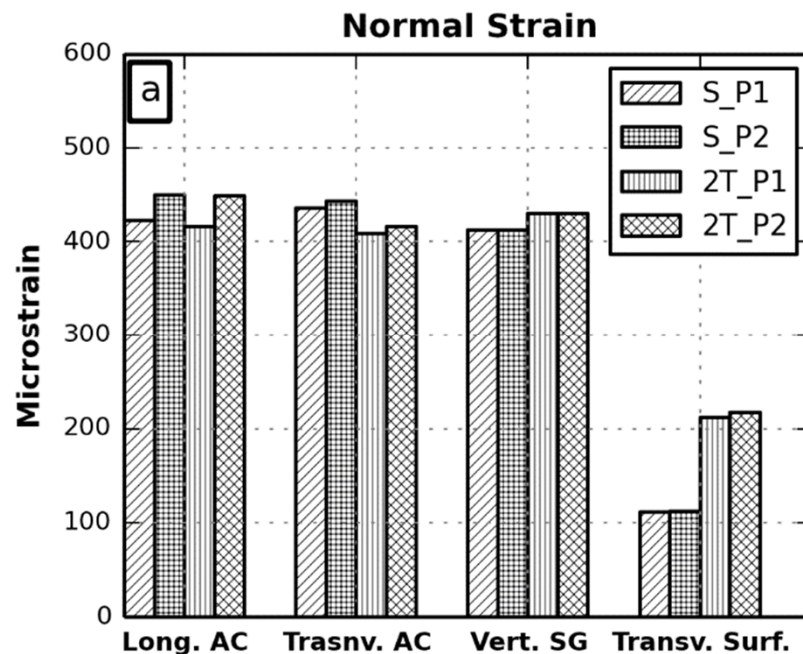


Shear Strain



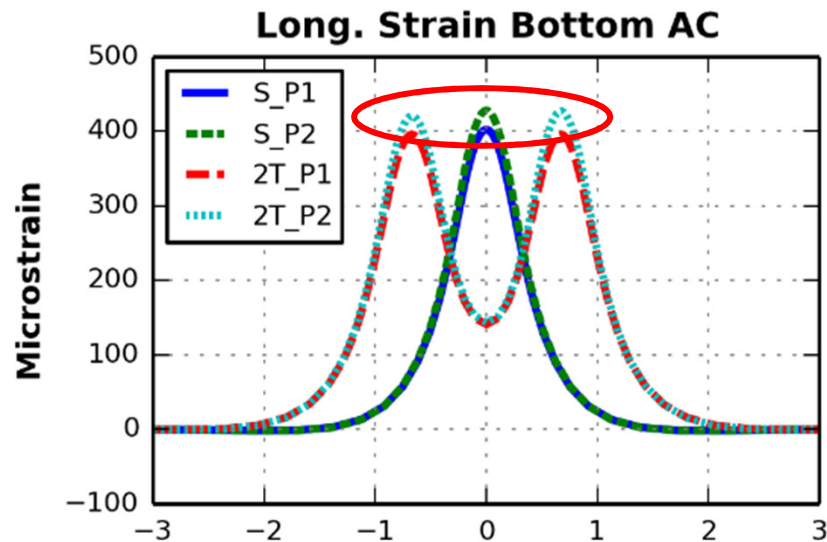
Gear and Inflation Pressure Effect

- **Gear configuration** mainly affected $\epsilon_{33.surf}$ and $\epsilon_{23.sg}$
- **Inflation pressure** relevant for $\epsilon_{11,ac}$



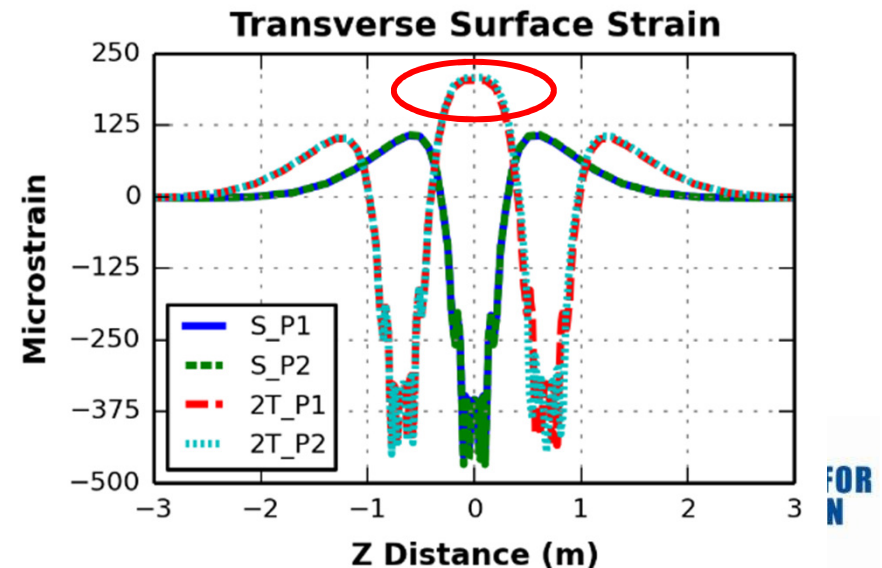
S=Single, 2T: Dual in tandem; P1=1.45 MPa; and P2=1.69 MPa

Transverse Variation Normal Strains

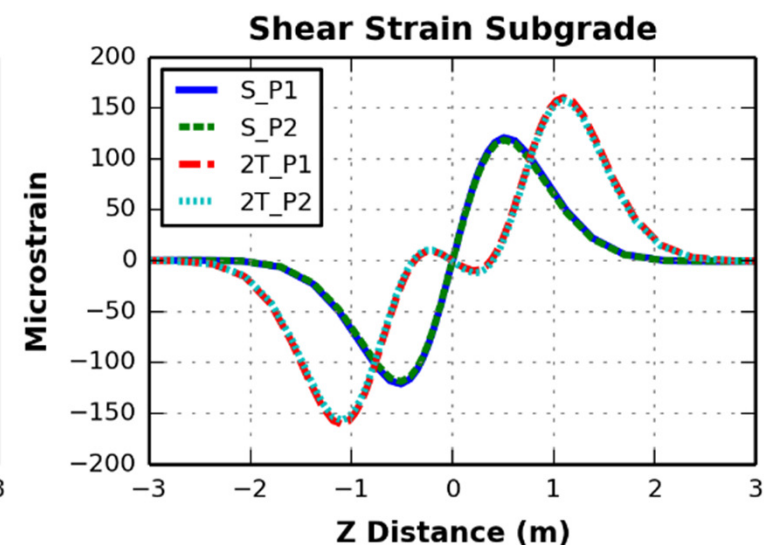
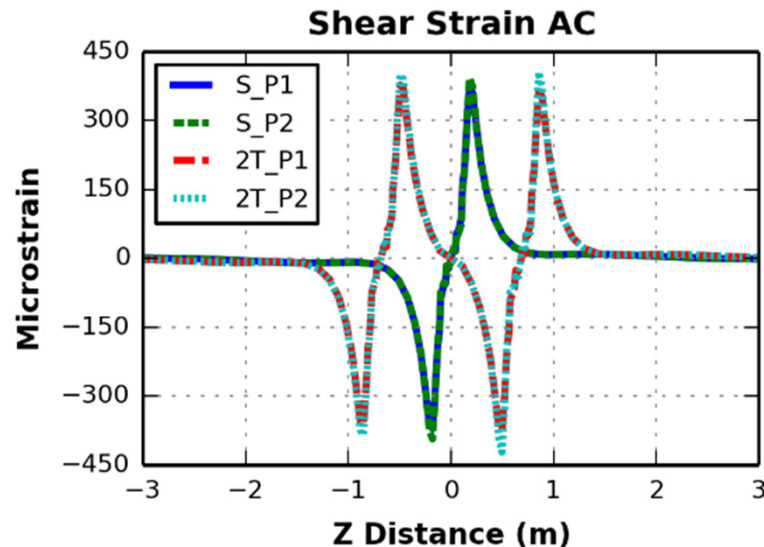


- Maximum $\epsilon_{33,surf}$ next to tire, then high influence of gear configuration

- Maximum $\epsilon_{11,ac}$ located under a tire, then low influence of gear configuration but higher effect of inflation pressure
- Similar behavior for $\epsilon_{22,sg}$ and ϵ_{33ac}



Transverse Variation Shear Strains

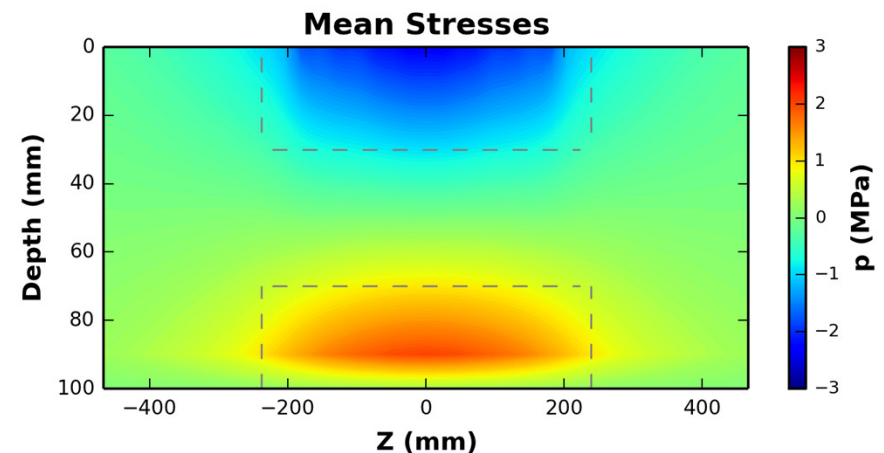
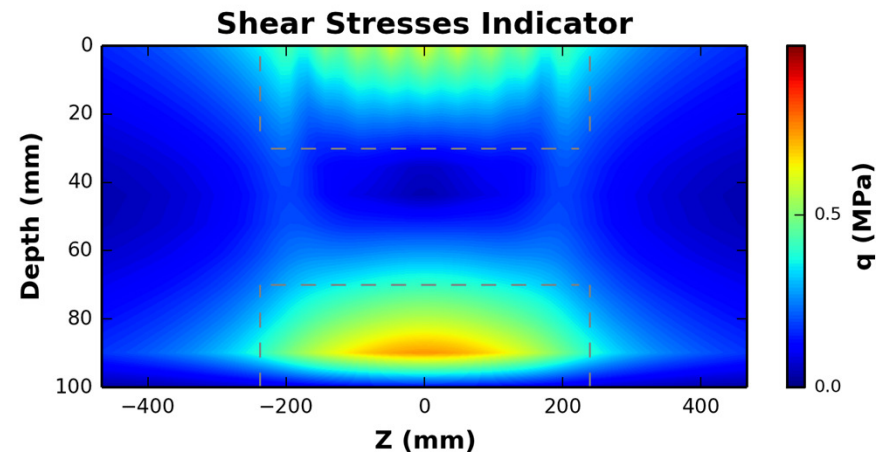
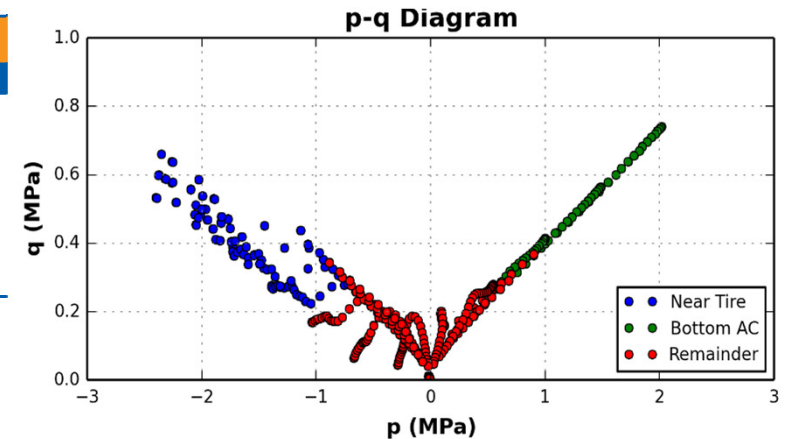


- In **AC**, shear strain was mainly affected by **inflation pressure**
- Location of maximum shear departs from tire's edge as depth increased
- **Shear strain in subgrade** was greatly influenced by **gear configuration**

Combined Stress Indicators

- **3D stresses** state provided better understanding of structural behavior
- **Isolated responses** (e.g. ε_{11}) cannot capture near-surface differences
- **Zone close to tire and at bottom of AC** are critical

$$p = \frac{1}{3}(\sigma_1 + \sigma_2 + \sigma_3);$$
$$q = \frac{1}{6}\sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_1 - \sigma_3)^2 + (\sigma_2 - \sigma_3)^2}$$



Final Remarks

- ❑ **Conventional pavement** analysis has significant **limitations**
- ❑ Analysis of airfield pavement should not be limited to tensile strain at bottom of AC and vertical strain on top of subgrade
- ❑ **Gear configuration** is relevant for transverse surface strain and shear strain in base and subgrade
- ❑ **Tire inflation pressure** mainly affected responses under the top 10 in

Future Work

- Model validation through airfield pavement **instrumentation**
- Model **contact stresses** at the tire-pavement interface
- Analysis of **combined stress/strain indicators** (e.g. octahedral shear stresses, mean stresses)
- Development of simplified tool to replace FEM (e.g. **Artificial Neural Networks**)

Acknowledgement

- ❑ This research was supported by the 2013-2014 **Graduate Research Award Program** on Public Sector - Aviation Issues from the **Airport Cooperative Research Program (ACRP)**
- ❑ **Randy Berg** of the Salk Lake City Dept of Airports and **Vivek Khanna** of the Ok Aeronautics Commission; **Lawrence Goldstein** of ACRP
- ❑ **Navneet Garg** of FAA Airport Technology R&D

QUESTIONS?
